

الرقم:	الفصل:	الاسم (باللغة العربية):
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- (1) A system to aid and control the walk of a partially disabled person could use automatic control of the walking system. One model of the system is shown in figure 2. Design a controller $G_c(s)$ such that the settling time to a unit step reference input is approximately 4 second.

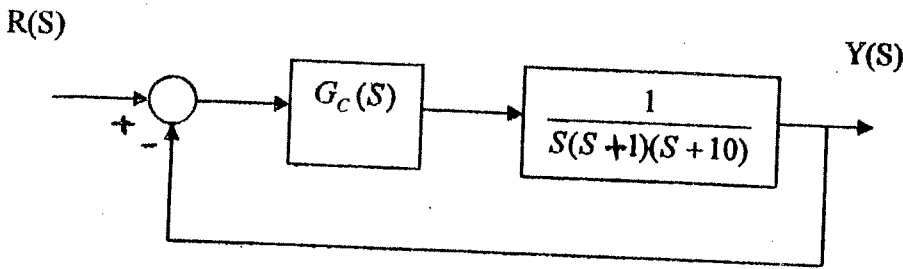


Figure 2

- Find the improvement in the steady state error due to a unit step reference input.
- Sketch the resulting time response to a unit step input.
- Comment on the effect of the controller $G_c(s)$ on the time response.
- If the system is subjected to a unit step disturbance input between the plant and the controller, find the improvement in the steady state error due to the unit step disturbance input.

Midterm Solution

Q1 Solution:

* To achieve the required settling time we will use a PD controller.

$$G_c(s) = K_p + K_d s$$

After adding the compensator, the characteristic equation will be $\frac{K_p + K_d s}{s(s+1)(s+10)} + 1 = 0$

$$s^3 + 11s^2 + (10 + K_d)s + K_p = 0 = (s + \alpha)(s^2 + 2\eta\omega_n s + \omega_n^2)$$

to have $t_s = 4 \text{ sec} = \frac{4}{2\eta\omega_n} \rightarrow \therefore \eta\omega_n = 1$ (1)

Comparing coefficients:

$$\alpha + 2\eta\omega_n = 11 \rightarrow \alpha = 9$$

$$\omega_n^2 + 2\eta\omega_n\alpha = 10 + K_d \rightarrow K_d = \omega_n^2 + 8$$
 (2)

$$\alpha\omega_n^2 = K_p \rightarrow K_p = 9\omega_n^2$$
 (3)

we have 3 equations in 4 unknowns (η, ω_n, K_p, K_d)
* As this application is for the aid of a disabled person the damping factor should be large enough to reduce the oscillations. So we will take $0.7 < \eta < 1$

\rightarrow for $\eta = 0.707 = \frac{1}{\sqrt{2}}$

$\hookrightarrow \omega_n = \sqrt{2} \text{ rad/sec}$

$\hookrightarrow K_d = 10$

$\hookrightarrow K_p = 18$

for $\eta = 1 \rightarrow \omega_n = 1 \text{ rad/sec}$

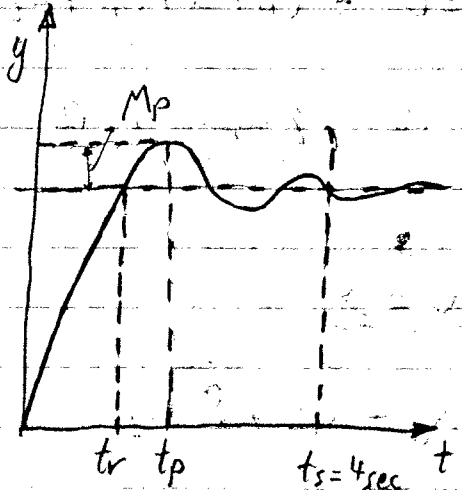
$$\begin{cases} \rightarrow K_d = 9 \\ \rightarrow K_p = 9 \end{cases}$$

★ Improvement in SS error for a Unit step input
→ the system is type 1 before & after the compensation, so the SS error for a Unit step is Zero in both cases.

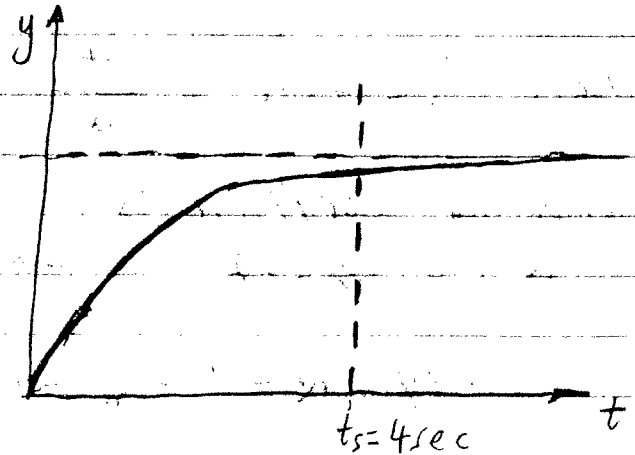
NO Improvement!

★ Sketch the resulting time response

$$\eta = \frac{1}{\sqrt{2}}$$



$$\eta = 1$$



$$M_p = 4.3\%$$

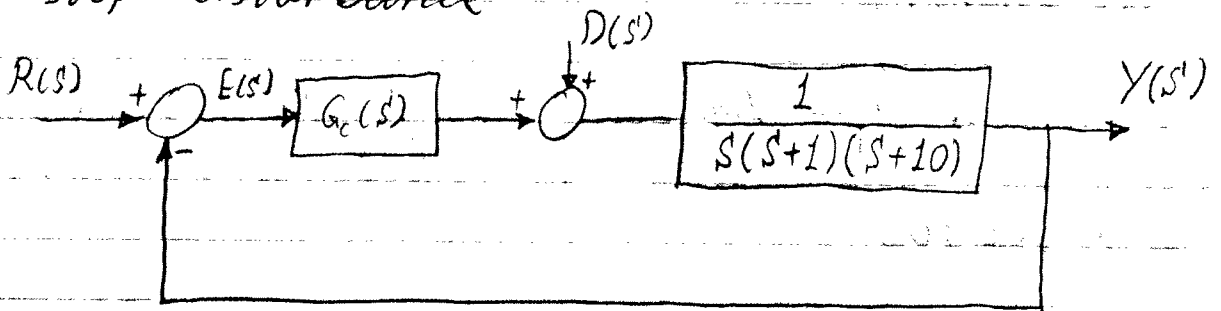
$$t_r = \frac{3}{4}\pi = 2.356 \text{ sec}$$

$$t_p = \pi = 3.14 \text{ sec}$$

Comments

The PD controller responds to the rate of change of the error. It adds damping to the system & improves the transient response. The PD controller has no direct effect on the steady state error.

* Unit step disturbance



let $R(s) = 0$

$$\frac{E(s)}{D(s)} = \frac{1}{1 + \frac{G_c(s)}{s(s+1)(s+10)}} = \frac{-1}{s^3 + 11s^2 + 10s + G_c(s)}$$

$e_{ss} = \lim_{s \rightarrow 0} s E(s)$ but $D(s) = \frac{1}{s}$

$\therefore e_{ss} = \lim_{s \rightarrow 0} \frac{E(s)}{D(s)} = \frac{1}{\lim_{s \rightarrow 0} G_c(s)}$

before compensation $G_c(s) = 1 \rightarrow e_{ss} = -1$

after compensation $G_c(s) = K_p + K_d s \rightarrow e_{ss} = \frac{-1}{K_p}$

$\eta = 1 \rightarrow e_{ss} = \frac{-1}{9}$

$\eta = \frac{1}{\sqrt{2}} \rightarrow e_{ss} = \frac{-1}{18}$

Improvement = $\frac{e_{ss} |_{\text{before}} - e_{ss} |_{\text{after}}}{e_{ss} |_{\text{before}}}$
 $= \frac{1 - \frac{1}{9}}{1}$

Improvement = $\frac{1 - \frac{1}{18}}{1}$

89% improvement in SS error due to unit step disturbance

94% improvement in SS error due to unit step disturbance

(2) The open loop transfer function of a unity feedback control system is

$$G(s) = \frac{K}{s(1+0.1s)(1+0.4s)}$$

- (a) Use the Bode plot to estimate the gain and phase margins of the system. Discuss the closed-loop stability
- (b) Design a lag-lead compensator so that the phase margin is at least 45° , and evaluate the system band-width before and after compensation.
- (c) The velocity constant, $K_v = 100 \text{ sec}^{-1}$

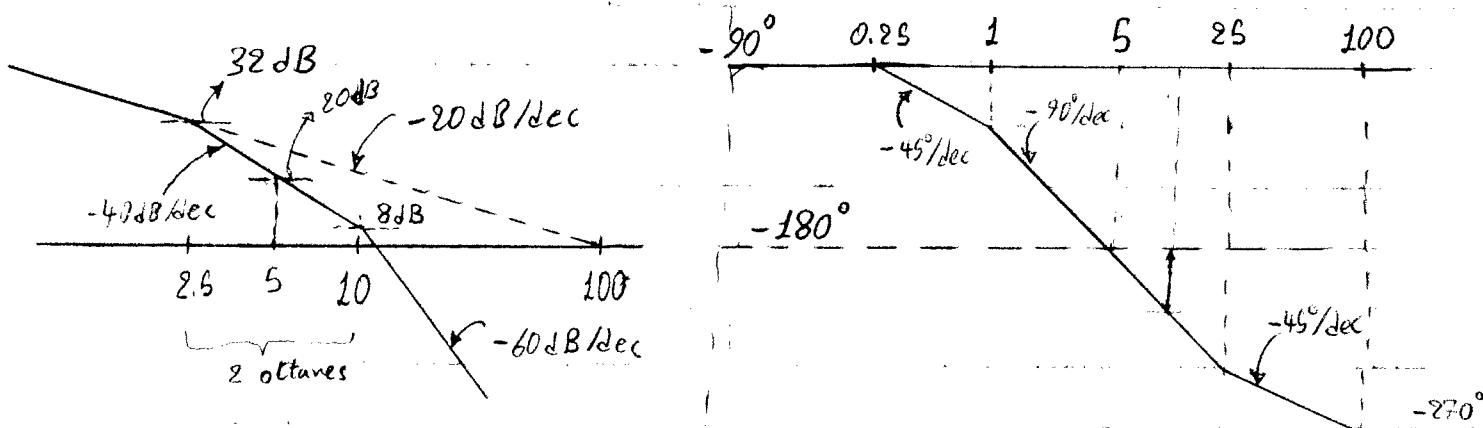
Q2 Solution :

* to have $K_v = 100 \text{ sec}^{-1}$ $\therefore \lim_{s \rightarrow 0} s^1 G(s) = 100$

$\therefore K = 100$

* Drawing the bode plot of $G(s) = \frac{100}{s(1+s/10)(1+s/2.5)}$

Corner frequencies @ $\omega = 10 \text{ rad/sec}$
& $\omega = 2.5 \text{ rad/sec}$



$\omega_{gc} = 13.6 \text{ rad/sec}$

$\omega_{pc} = 5 \text{ rad/sec}$

GM = -20 dB

PM = -39°

System is unstable

* We will use a lead-lag compensator to achieve the desired 45° phase margin.

* Two solutions are shown and both will be considered correct.

Solution #1

Assumptions:

* $\omega_{gc_new} = \omega_{pc_old} = 5 \text{ rad/sec}$

* $B = \frac{1}{\alpha} = 10$

* We want to calculate τ_{lead}, τ_{lag}

$\frac{1}{\tau_{lag}} = 0.1 \omega_{gc_new} \rightarrow \tau_{lag} = 2 \text{ sec}$

$\rightarrow \text{gain @ } \omega_{gc_new} = a = 20 \text{ dB}$

$\therefore -a = -20 \text{ dB}$

$\therefore \frac{1}{\tau_{lead}} = \omega_{gc_new}$

$\therefore \tau_{lead} = 0.2 \text{ sec}$

$G_c(s) = \frac{(1+2s)(1+0.2s)}{(1+20s)(1+0.02s)}$

Check for PM

$PM = 180 + \angle G(j\omega_{gc_new})$

$PM_{new} = 34.15^\circ$



OK!

Solution #2

Assumptions:

* $\omega_{gc_new} = \omega_{pc_old} = 5 \text{ rad/sec}$

$\alpha \neq 1/10$

Phase @ $\omega_{gc_new} = -180^\circ$

to have $PM = 45^\circ$

we need

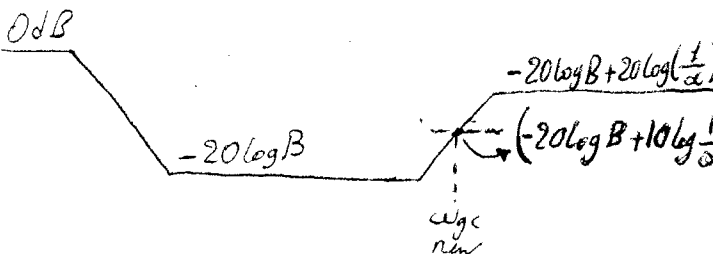
$\phi = 45 + 12 = 57^\circ > 45^\circ$

Correction

we will take $\alpha = 0.1$

$\rightarrow \phi \approx 55^\circ$
still OK

gain @ $\omega_{gc_new} = a = 20 \text{ dB}$



$a - 20 \log B + 10 \log(\frac{1}{\alpha}) = 0 \text{ dB}$

$\therefore B = 31.623 \text{ rad/sec}$

$\tau_{lag} = \frac{1}{0.1 \omega_{gc_new}} = 2 \text{ sec}$

$\frac{1}{\tau_{lead} \sqrt{\alpha}} = \omega_{gc_new} \rightarrow \tau_{lead} = 0.6325 \text{ sec}$

$G_c(s) = \frac{(1+2s)(1+0.6325s)}{(1+63.246s)(1+0.06325s)}$

$PM_{new} = 49.37^\circ$



OK!