

Topic 4

Linear Wire and Small Circular Loop Antennas

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Linear Wire Antennas and Small Circular Loop Antenna

- 1 Infinitesimal Dipole
- 2 Small Dipole
- 3 Finite Length Dipole
- 4 Conductor Losses and Loss Resistance
- 5 Linear Elements Near or on Infinite Conductor
- 6 Loop Antennas

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Infinitesimal Dipole

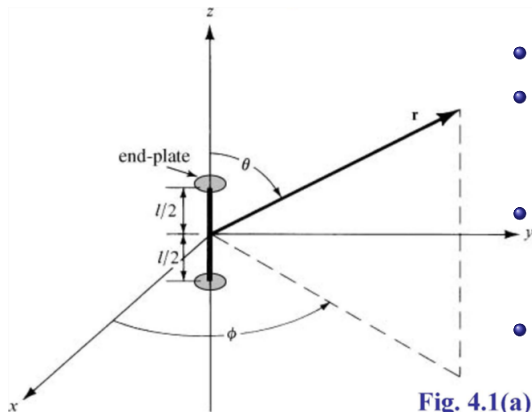


Fig. 4.1(a)

$$\mathbf{A}(r, \theta, \phi) = \frac{\mu}{4\pi} \int_C \mathbf{l}_e \frac{e^{-jkR}}{R} dl' = \hat{\mathbf{a}}_z \frac{\mu I_0 l}{4\pi r} e^{-jkr}$$

- $l \ll \lambda$ ($l \leq \lambda/50$)
- End plates are to maintain uniform current, however they are very small to affect radiation!
- Not very practical, however they are considered as a basic building blocks for complex structures.
- $\mathbf{l}_e(z') = \hat{\mathbf{a}}_z I_0$

Infinitesimal Dipole

- Transformation from rectangular spherical components,

$$\begin{bmatrix} A_r \\ A_\theta \\ A_\phi \end{bmatrix} = \begin{bmatrix} \sin \theta \cos \phi & \sin \theta \sin \phi & \cos \theta \\ \cos \theta \cos \phi & \cos \theta \sin \phi & -\sin \theta \\ -\sin \phi & \cos \phi & 0 \end{bmatrix} \begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix}$$

$$A_r = \frac{\mu I_0 l e^{-jkr}}{4\pi r} \cos \theta, \quad A_\theta = -\frac{\mu I_0 l e^{-jkr}}{4\pi r} \sin \theta$$

- Magnetic field

$$\mathbf{H} = \frac{1}{\mu} \nabla \times \mathbf{A} = \mathbf{a}_\phi \frac{1}{\mu r} \left[\frac{\partial}{\partial r} (rA_\theta) - \frac{\partial A_r}{\partial \theta} \right] = j \frac{k I_0 l e^{-jkr}}{4\pi r} \sin \theta \left[1 + \frac{1}{jkr} \right] \mathbf{a}_\phi$$

- Electric field

$$\mathbf{E} = \frac{1}{j\omega\epsilon} \nabla \times \mathbf{H}$$

Infinitesimal Dipole

$$\mathbf{E} = j\eta \frac{kl_0 I}{4\pi r} e^{-jkr} \left[2\cos\theta \left(\frac{1}{jkr} - \frac{1}{k^2 r^2} \right) \mathbf{a}_r + \sin\theta \left(1 + \frac{1}{jkr} - \frac{1}{k^2 r^2} \right) \mathbf{a}_\theta \right]$$

$$\mathbf{H} = j \frac{kl_0 I e^{-jkr}}{4\pi r} \sin\theta \left[1 + \frac{1}{jkr} \right] \mathbf{a}_\phi$$

- Radiation Power Density,

$$\mathbf{W} = \frac{1}{2} (\mathbf{E} \times \mathbf{H}^*) = \frac{1}{2} (\mathbf{a}_r E_\theta H_\phi^* - \mathbf{a}_\theta E_r H_\phi^*)$$

- Radiated Power,

$$\begin{aligned} P_{\text{rad}} &= \Re \left\{ \oiint_S \mathbf{W} \cdot d\mathbf{s} \right\} = \eta \frac{k^2 I_0^2 I^2}{32\pi^2} \int_0^{2\pi} d\phi \int_0^\pi \sin^2\theta \sin\theta d\theta \\ &= \frac{\eta\pi}{4} \left| I_0 \frac{l}{\lambda} \right|^2 \left[-\cos\theta + \frac{\cos^3\theta}{3} \right]_0^\pi = \frac{\eta\pi}{3} \left| I_0 \frac{l}{\lambda} \right|^2 \end{aligned}$$

- Radiation Resistance

$$P_{\text{rad}} = \frac{\eta\pi}{3} \left| I_0 \frac{l}{\lambda} \right|^2 = \frac{1}{2} |I_0|^2 R_r \quad \Rightarrow \quad R_r = 80\pi^2 \left(\frac{l}{\lambda} \right)^2$$

Radiation Regions

- Near field region $kr \ll 1$,

$$\mathbf{E} = -j\eta \frac{l_0 I}{4\pi kr^3} e^{-jkr} [2 \cos \theta \mathbf{a}_r + \sin \theta \mathbf{a}_\theta]$$

$$\mathbf{H} = \frac{l_0 I e^{-jkr}}{4\pi r^2} \sin \theta \mathbf{a}_\phi$$

- Intermediate-field (Fresnel) region $kr > 1$,

$$\mathbf{E} = j\eta \frac{kl_0 I}{4\pi r} e^{-jkr} \left[\frac{2}{jkr} \cos \theta \mathbf{a}_r + \sin \theta \mathbf{a}_\theta \right]$$

$$\mathbf{H} = j \frac{kl_0 I e^{-jkr}}{4\pi r} \sin \theta \mathbf{a}_\phi$$

- Far-field (Fraunhofer) region $kr \gg 1$,

$$\mathbf{E} = j\eta \frac{kl_0 I \sin \theta}{4\pi r} e^{-jkr} \mathbf{a}_\theta, \quad \mathbf{H} = j \frac{kl_0 I e^{-jkr}}{4\pi r} \sin \theta \mathbf{a}_\phi$$

$$\mathbf{H} = \frac{1}{\eta} \mathbf{a}_r \times \mathbf{E}$$

$$W_{\text{rad}} = \frac{|E_{\theta}|^2}{2\eta}$$

$$U = r^2 W_{\text{rad}} = r^2 \frac{|E_{\theta}|^2}{2\eta} = \eta \frac{k^2 I_0^2 l^2}{32\pi^2} \sin^2 \theta = \frac{\eta}{8} \left| I_0 \frac{l}{\lambda} \right|^2 \sin^2 \theta$$

$$P_{\text{rad}} = \frac{\eta\pi}{3} \left| I_0 \frac{l}{\lambda} \right|^2$$

$$D = \frac{4\pi U}{P_{\text{rad}}} = 1.5 \sin^2 \theta$$

Outline

- 1 Infinitesimal Dipole
- 2 Small Dipole**
- 3 Finite Length Dipole
- 4 Conductor Losses and Loss Resistance
- 5 Linear Elements Near or on Infinite Conductor
- 6 Loop Antennas

Small Dipole

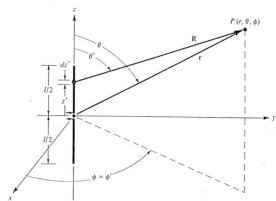
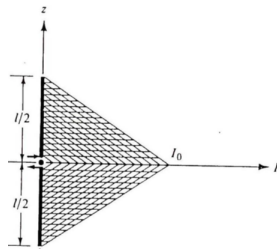
$$I_e(z') = \begin{cases} \mathbf{a}_z I_0 \left(1 - \frac{2z'}{l}\right) & 0 \leq z' \leq l/2 \\ \mathbf{a}_z I_0 \left(1 + \frac{2z'}{l}\right) & -l/2 \leq z' \leq 0 \end{cases}$$

$$\mathbf{A} = \mathbf{a}_z \frac{1}{2} \left[\frac{\mu I_0 l e^{-jkr}}{4\pi r} \right]$$

$$\mathbf{E} = j\eta \frac{kl_0 (l/2) e^{-kr}}{4\pi r} \sin\theta \mathbf{a}_\theta$$

$$\mathbf{H} = j \frac{kl_0 (l/2) e^{-kr}}{4\pi r} \sin\theta \mathbf{a}_\phi$$

- Radiation resistance $R_r = 80\pi^2 \left(\frac{l/2}{\lambda}\right)^2$

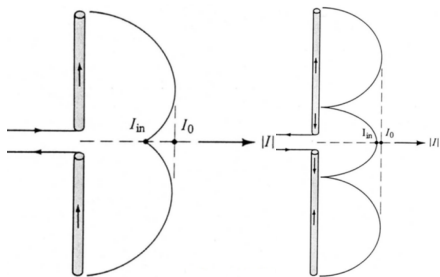
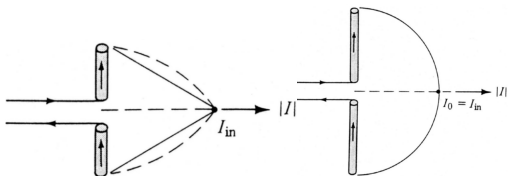
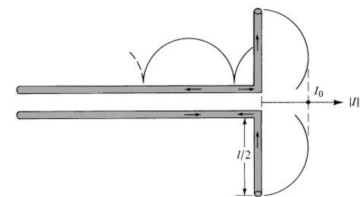
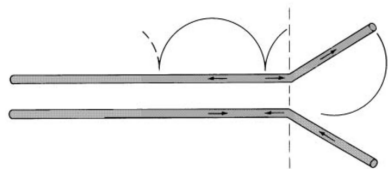
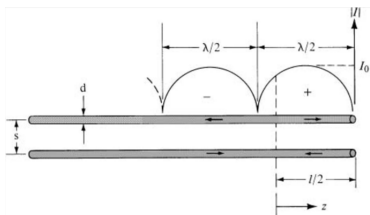


Small dipole of length l is equivalent to infinitesimal dipole of length $l/2$.

Outline

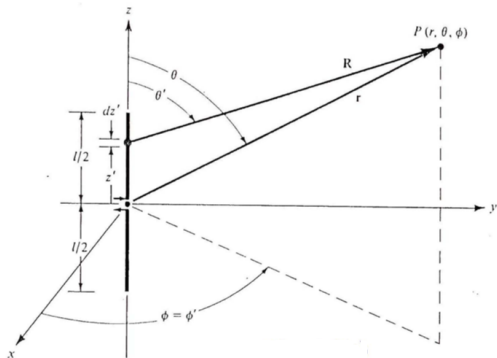
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Finite Length Dipole



$$\mathbf{l}_e(z') = \begin{cases} \mathbf{a}_z I_0 \sin \left[k \left(\frac{l}{2} - z' \right) \right], & 0 \leq z' \leq \frac{l}{2} \\ \mathbf{a}_z I_0 \sin \left[k \left(\frac{l}{2} + z' \right) \right], & -\frac{l}{2} \leq z' \leq 0 \end{cases}$$

Finite Length Dipole



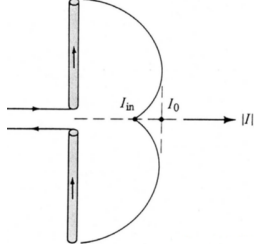
$$\mathbf{E} \simeq -j\omega [A_\theta \mathbf{a}_\theta + A_\phi \mathbf{a}_\phi],$$

$$\mathbf{A}(r, \theta, \phi) \simeq \frac{\mu}{4\pi} \frac{e^{-jkr}}{r} \int_C I_e(r', \theta', \phi') e^{j\mathbf{k} \cdot \mathbf{r}'} dl'$$

$$\mathbf{A} = \frac{\mu}{4\pi} \frac{e^{-jkr}}{r} \int_{-l/2}^{l/2} I_e(z') e^{jkz' \cos \theta} dz' \mathbf{a}_z$$

$$\mathbf{E} = j\eta \frac{ke^{-jkr}}{4\pi r} \sin \theta \int_{-l/2}^{l/2} I_e(z') e^{jkz' \cos \theta} dz' \mathbf{a}_\theta$$

$$I_e(z') = \begin{cases} \mathbf{a}_z I_0 \sin \left[k \left(\frac{l}{2} - z' \right) \right], & 0 \leq z' \leq \frac{l}{2} \\ \mathbf{a}_z I_0 \sin \left[k \left(\frac{l}{2} + z' \right) \right], & -\frac{l}{2} \leq z' \leq 0 \end{cases}$$



$$\mathbf{E} = j\eta \frac{ke^{-jkr}}{4\pi r} \sin \theta \int_{-l/2}^{l/2} I_e(z') e^{jkz' \cos \theta} dz' \mathbf{a}_\theta$$

$$\begin{aligned} \mathbf{E} = & j\eta \frac{kl_0 e^{-jkr}}{4\pi r} \sin \theta \left\{ \int_{-l/2}^0 \sin \left[k \left(\frac{l}{2} + z' \right) \right] e^{jkz' \cos \theta} dz' \right. \\ & \left. + \int_0^{l/2} \sin \left[k \left(\frac{l}{2} - z' \right) \right] e^{jkz' \cos \theta} dz' \right\} \mathbf{a}_\theta \end{aligned}$$

The integrals can be evaluated using

$$\int e^{\alpha x} \sin(\beta x + \gamma) dx = \frac{e^{\alpha x}}{\alpha^2 + \beta^2} [\alpha \sin(\beta x + \gamma) - \beta \cos(\beta x + \gamma)]$$

$$\mathbf{E} = j\eta \frac{l_0 e^{-jkr}}{2\pi r} \left[\frac{\cos \left(\frac{kl}{2} \cos \theta \right) - \cos \left(\frac{kl}{2} \right)}{\sin \theta} \right] \mathbf{a}_\theta$$

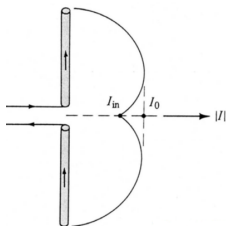
Radiation Intensity, and Radiation Resistance

$$U = \frac{r^2}{2\eta} |E_\theta|^2 = \frac{\eta |I_0|^2}{8\pi^2} \left[\frac{\cos\left(\frac{kl}{2} \cos\theta\right) - \cos\left(\frac{kl}{2}\right)}{\sin\theta} \right]^2$$

$$P_{\text{rad}} = \int_0^{2\pi} \int_0^\pi U \sin\theta d\theta d\phi = \frac{\eta |I_0|^2}{4\pi} \int_0^\pi \left[\frac{\cos\left(\frac{kl}{2} \cos\theta\right) - \cos\left(\frac{kl}{2}\right)}{\sin\theta} \right]^2 d\theta$$

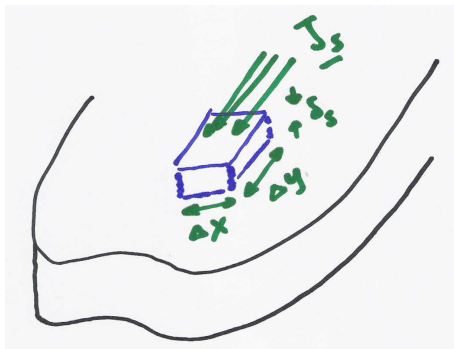
$$P_{\text{rad}} = \frac{1}{2} |I_{\text{in}}|^2 R_r = \frac{1}{2} |I_0|^2 \sin^2(kl/2) R_r$$

$$R_r = \frac{1}{\sin^2(kl/2)} \frac{\eta}{2\pi} \int_0^\pi \left[\frac{\cos\left(\frac{kl}{2} \cos\theta\right) - \cos\left(\frac{kl}{2}\right)}{\sin\theta} \right]^2 d\theta$$



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Skin depth:

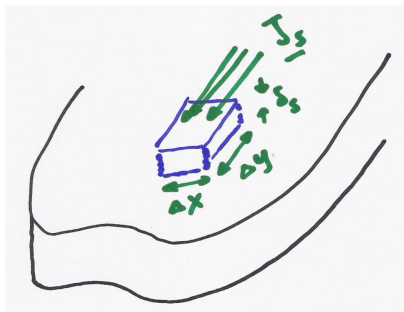
$$\delta_s = 1/\sqrt{\pi f \mu \sigma}$$

- Resistance of the segment with dimensions $(\Delta x, \Delta y, \delta_s)$:

$$R = \frac{\Delta y}{\sigma \delta_s \Delta x}$$

- Current flowing through length Δx : $\Delta I_s = |\mathbf{J}_s| \Delta x$

Conductor Losses



$$R = \frac{\Delta y}{\sigma \delta_s \Delta x}$$

- Current flowing through length Δx : $\Delta I_s = |\mathbf{J}_s| \Delta x$

- Power loss in the area $\Delta x \Delta y$,

$$\Delta P_{loss} = \frac{1}{2} |\Delta I_s|^2 R = \frac{1}{2} |\mathbf{J}_s|^2 \frac{1}{\sigma \delta_s} \Delta x \Delta y$$

- Total Power loss in a conductor area S ,

$$P_{loss} = \frac{1}{2} \int_S |\mathbf{J}_s|^2 R_s ds, \quad \text{where } R_s = \frac{1}{\sigma \delta_s} = \sqrt{\frac{\pi f \mu}{\sigma}}$$

Conductor Losses

$$P_{loss} = \frac{1}{2} \int_S |\mathbf{J}_s|^2 R_s ds, \quad \text{where } R_s = \frac{1}{\sigma \delta_s} = \sqrt{\frac{\pi f \mu}{\sigma}}$$

R_s is called the *surface resistance* of the conductor.

- The surface current can be obtained using the approximation of a perfect conductor boundary conditions,

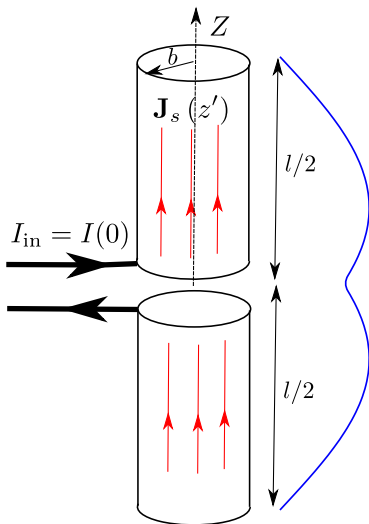
$$\mathbf{J}_s = \mathbf{n} \times \mathbf{H} \quad \implies \quad |\mathbf{J}_s| = |\mathbf{H}|$$

where \mathbf{n} is the normal unit vector on the conductor.

- Total Power loss in a conductor area S ,

$$P_{loss} = \frac{1}{2} \int_S |\mathbf{H}|^2 R_s ds, \quad \text{where } R_s = \frac{1}{\sigma \delta_s} = \sqrt{\frac{\pi f \mu}{\sigma}}$$

Loss resistance



$$\begin{aligned} P_{\text{loss}} &= \frac{1}{2} \int_S |\mathbf{J}_s|^2 R_s ds \\ &= \frac{1}{2} \int_{-l/2}^{l/2} \frac{|I_e(z')|^2}{(2\pi b)^2} R_s (2\pi b) dz' \end{aligned}$$

$$P_{\text{loss}} = \frac{1}{2} \int_{-l/2}^{l/2} \frac{|I_e(z')|^2}{2\pi b} R_s dz' = \frac{1}{2} |I_e(0)|^2 R_L$$

$$R_L = \frac{R_s}{2\pi b} \int_{-l/2}^{l/2} \left| \frac{I_e(z')}{I_e(0)} \right|^2 dz'$$

Half-wavelength ($\lambda/2$) dipole

$$U = \frac{r^2}{2\eta} |E_\theta|^2 = \frac{\eta |I_0|^2}{8\pi^2} \left[\frac{\cos\left(\frac{\pi}{2} \cos\theta\right)}{\sin\theta} \right]^2$$

$$P_{\text{rad}} = \int_0^{2\pi} \int_0^\pi U \sin\theta d\theta d\phi = \frac{\eta |I_0|^2}{4\pi} \int_0^\pi \frac{\cos^2\left(\frac{\pi}{2} \cos\theta\right)}{\sin\theta} d\theta$$

$$P_{\text{rad}} = \frac{1}{2} |I_0|^2 R_r$$

$$R_r = \frac{\eta}{2\pi} \int_0^\pi \frac{\cos^2\left(\frac{\pi}{2} \cos\theta\right)}{\sin\theta} d\theta = 73 \Omega$$

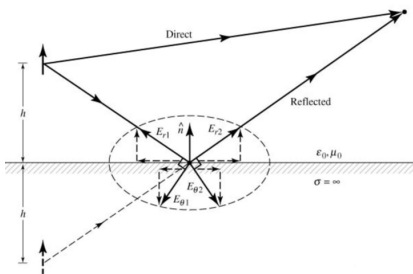
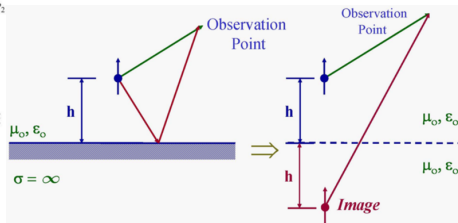
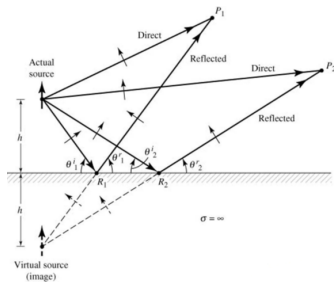
$$D = \frac{4\pi U}{P_{\text{rad}}} = \frac{\eta}{\pi R_r} \left[\frac{\cos\left(\frac{\pi}{2} \cos\theta\right)}{\sin\theta} \right]^2 = 1.64 \left[\frac{\cos\left(\frac{\pi}{2} \cos\theta\right)}{\sin\theta} \right]^2$$

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Linear Elements Near or on Infinite Conductor

Image Theory

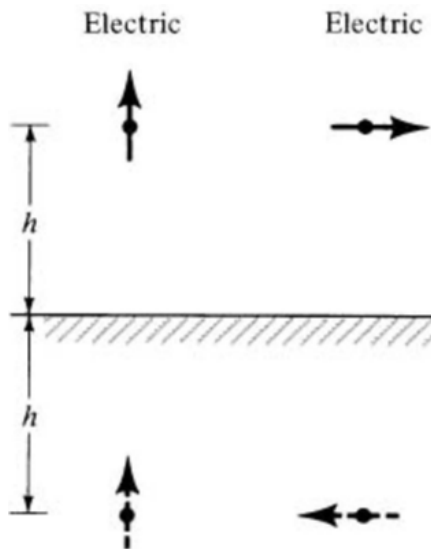


$$\mathbf{E} = \frac{j\eta k l_0 e^{-jkr}}{4\pi r} \left[\cos\theta \left(\frac{2}{jkr} - \frac{1}{k^2 r^2} \right) \mathbf{a}_r + \sin\theta \left(1 + \frac{1}{jkr} - \frac{1}{k^2 r^2} \right) \mathbf{a}_\theta \right]$$

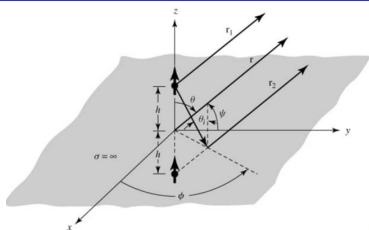
$$\mathbf{H} = j \frac{k l_0 e^{-jkr}}{4\pi r} \sin\theta \left[1 + \frac{1}{jkr} \right] \mathbf{a}_\phi$$

Linear Elements Near or on Infinite Conductor

Image Theory



Vertical Infinitesimal Dipole Above Ground Plane



$$\mathbf{A}(r, \theta, \phi) \simeq \frac{\mu}{4\pi} \frac{e^{-jkr}}{r} \int_C I_e e^{j\mathbf{k} \cdot \mathbf{r}'} dl'$$

$$\mathbf{H} \simeq \frac{\mathbf{a}_r \times \mathbf{E}}{\eta}, \quad \mathbf{E} \simeq -j\omega [A_\theta \mathbf{a}_\theta + A_\phi \mathbf{a}_\phi]$$

$$\mathbf{E} = \begin{cases} j\eta \frac{kl_0 I_e e^{-kr}}{4\pi r} \sin \theta [2 \cos(kh \cos \theta)] \mathbf{a}_\theta & z \geq 0 \\ \mathbf{0} & z < 0 \end{cases}$$

$$U = \begin{cases} \frac{\eta}{2} \left| \frac{l_0 I_e}{\lambda} \right|^2 \sin^2 \theta \cos^2(kh \cos \theta) & 0 < \theta \leq \pi/2 \\ 0 & \pi/2 < \theta \leq \pi \end{cases}$$

$$\begin{aligned} P_{\text{rad}} &= \int U d\Omega = \pi\eta \left| \frac{l_0 I_e}{\lambda} \right|^2 \int_0^{\pi/2} \sin^3 \theta \cos^2(kh \cos \theta) d\theta \\ &= \pi\eta \left| \frac{l_0 I_e}{\lambda} \right|^2 \int_0^1 (1-x^2) \cos^2(khx) dx \end{aligned}$$

Vertical Infinitesimal Dipole Above Ground Plane

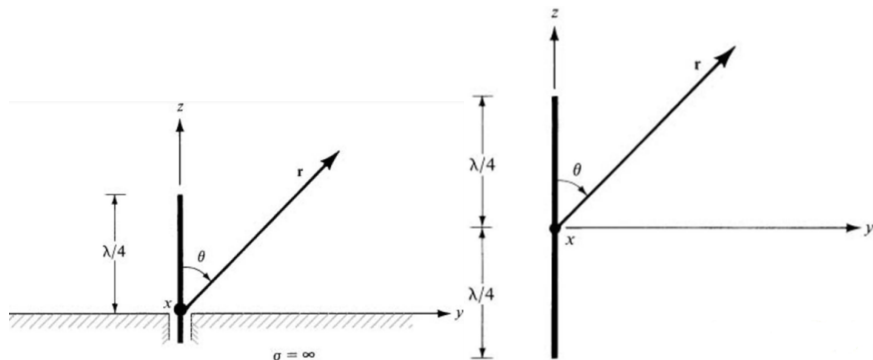
$$P_{\text{rad}} = \pi\eta \left| \frac{I_0 l}{\lambda} \right|^2 \left[\frac{1}{3} - \frac{\cos(2kh)}{(2kh)^2} + \frac{\sin(2kh)}{(2kh)^3} \right]$$

$$U_{\text{max}} = \frac{\eta}{2} \left| \frac{I_0 l}{\lambda} \right|^2 \quad \Rightarrow \quad D_0 = \frac{4\pi U_{\text{max}}}{P_{\text{rad}}} = \frac{2}{\left[\frac{1}{3} - \frac{\cos(2kh)}{(2kh)^2} + \frac{\sin(2kh)}{(2kh)^3} \right]}$$

$$R_r = 2\pi\eta \left(\frac{l}{\lambda} \right)^2 \left[\frac{1}{3} - \frac{\cos(2kh)}{(2kh)^2} + \frac{\sin(2kh)}{(2kh)^3} \right]$$

- $kh \rightarrow \infty$, $R_r = 80\pi^2 (l/\lambda)^2$, R_r is identical to *isolated Infinitesimal dipole*.
- $kh \rightarrow 0$, $D_0 = 3$, $R_r = 160\pi^2 (l/\lambda)^2$, D_0 and R_r are twice the *isolated Infinitesimal dipole*.

$\lambda/4$ Monopole on Infinite Electric Conductor



The radiation fields are identical in the upper half plane ($z > 0$). However the total radiated for the monopole is half its value for the dipole.

$$P_{\text{rad (m)}} = \frac{1}{2} P_{\text{rad (d)}}$$

$$D_m = 2D_d, \quad R_r \text{ (m)} = \frac{1}{2} R_r \text{ (d)}$$

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Angle Between Two Directions in Space

- The unit vector describing the the direction (θ, ϕ) ,

$$\mathbf{a}_r = \sin \theta \cos \phi \mathbf{a}_x + \sin \theta \sin \phi \mathbf{a}_y + \cos \theta \mathbf{a}_z$$

- The unit vector describing the the direction (θ', ϕ') ,

$$\mathbf{a}_{r'} = \sin \theta' \cos \phi' \mathbf{a}_x + \sin \theta' \sin \phi' \mathbf{a}_y + \cos \theta' \mathbf{a}_z$$

- The angle ψ between the two directions,

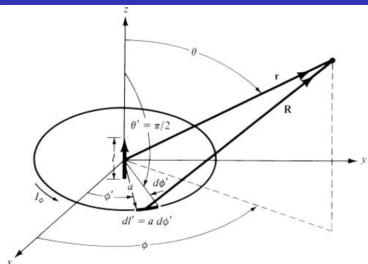
$$\cos \psi = \mathbf{a}_r \cdot \mathbf{a}_{r'}$$

$$\cos \psi = \sin \theta \sin \theta' \cos (\phi - \phi') + \cos \theta \cos \theta'$$

Small Circular Loop

Circumference $C < \frac{\lambda}{10}$

$$\mathbf{A}(r, \theta, \phi) = \frac{\mu}{4\pi} \int_C \mathbf{l}_e \frac{e^{-jkR}}{R} dl'$$



The source current is along $\hat{\mathbf{a}}_{\phi'}$: $\mathbf{l}_e = I_0 \hat{\mathbf{a}}_{\phi'}$. Transforming to Cartesian coordinates,

$$I_x = -I_0 \sin \phi',$$

$$I_y = I_0 \cos \phi'$$

Transforming to the spherical coordinates at the observation point,

$$I_r = I_x \cos \phi \sin \theta + I_y \sin \phi \sin \theta$$

$$I_\theta = I_x \cos \phi \cos \theta + I_y \sin \phi \cos \theta$$

$$I_\phi = -I_x \sin \phi + I_y \cos \phi$$

Small Circular Loop

$$I_x = -I_0 \sin \phi',$$

$$I_y = I_0 \cos \phi'$$

Transforming to the spherical coordinates at the observation point,

$$I_r = I_x \cos \phi \sin \theta + I_y \sin \phi \sin \theta$$

$$I_\theta = I_x \cos \phi \cos \theta + I_y \sin \phi \cos \theta$$

$$I_\phi = -I_x \sin \phi + I_y \cos \phi$$

$$I_r = I_0 \sin \theta \sin (\phi - \phi')$$

$$I_\theta = I_0 \cos \theta \sin (\phi - \phi')$$

$$I_\phi = I_0 \cos (\phi - \phi')$$

$$\mathbf{l}_e = \mathbf{a}_r I_0 \sin \theta \sin (\phi - \phi') + \mathbf{a}_\theta I_0 \cos \theta \sin (\phi - \phi') + \mathbf{a}_\phi I_0 \cos (\phi - \phi')$$

Small Circular Loop

$$\mathbf{A} = A_\phi \mathbf{a}_\phi, \quad A_\phi = \frac{\mu I_0 a}{4\pi} \int_0^{2\pi} \cos(\phi - \phi') \frac{e^{-jk\sqrt{r^2 + a^2 - 2ar \sin \theta \cos(\phi - \phi')}}}{\sqrt{r^2 + a^2 - 2ar \sin \theta \cos(\phi - \phi')}} d\phi'$$

$$f = \frac{e^{-jk\sqrt{r^2 + a^2 - 2ar \sin \theta \cos(\phi - \phi')}}}{\sqrt{r^2 + a^2 - 2ar \sin \theta \cos(\phi - \phi')}}}$$

$$f(a) \simeq f(0) + f'(0)a$$

$$f(0) = \frac{e^{-jkr}}{r}, \quad f'(0) = \frac{e^{-jkr}}{r^2} (jkr + 1) \sin \theta \cos(\phi - \phi')$$

$$f = \frac{e^{-jkr}}{r} \left[1 + a \left(\frac{1}{r} + jk \right) \sin \theta \cos(\phi - \phi') \right]$$

$$A_\phi = \frac{\mu I_0 a}{4\pi} \frac{e^{-jkr}}{r} \int_0^{2\pi} \cos(\phi - \phi') \left[1 + a \left(\frac{1}{r} + jk \right) \sin \theta \cos(\phi - \phi') \right] d\phi'$$

$$A_\phi = \frac{a^2 jk \mu I_0}{4} \frac{e^{-jkr}}{r} \left(\frac{1}{jkr} + 1 \right) \sin \theta$$

Small Circular Loop

$$\mathbf{A} = A_\phi \hat{\mathbf{a}}_\phi,$$

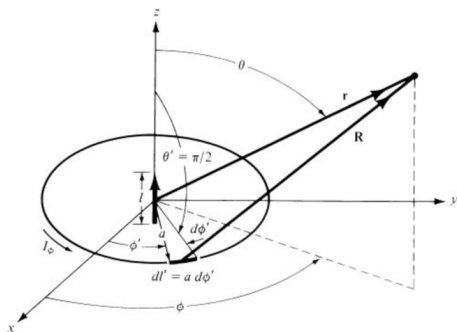
$$A_\phi = \frac{a^2 j k \mu I_0}{4} \frac{e^{-jkr}}{r} \left(\frac{1}{jkr} + 1 \right) \sin \theta$$

$$\mathbf{H} = \frac{1}{\mu} \nabla \times \mathbf{A},$$

$$\mathbf{E} = \frac{1}{j\omega\epsilon} \nabla \times \mathbf{H} = \frac{\eta}{jk} \nabla \times \mathbf{H}$$

$$\mathbf{H} = -\frac{(ka)^2 I_0 e^{-jkr}}{4r} \left[\left(\frac{2}{jkr} - \frac{2}{(kr)^2} \right) \cos \theta \hat{\mathbf{a}}_r + \left(-\frac{1}{(kr)^2} + \frac{1}{jkr} + 1 \right) \sin \theta \hat{\mathbf{a}}_\theta \right]$$

$$\mathbf{E} = \eta \frac{(ka)^2 I_0 e^{-jkr}}{4r} \left(\frac{1}{jkr} + 1 \right) \sin \theta \hat{\mathbf{a}}_\phi$$



Small Circular Loop

- Far Fields,

$$\mathbf{H} = -\frac{(ka)^2 I_0 e^{-jkr}}{4r} \sin \theta \mathbf{a}_\theta, \quad \mathbf{E} = \eta \frac{(ka)^2 I_0 e^{-jkr}}{4r} \sin \theta \mathbf{a}_\phi$$

- Radiated Power and Radiation Resistance

$$U = \eta \frac{(ka)^4 |I_0|^2}{32} \sin^2 \theta, \quad P_{\text{rad}} = \int U d\Omega = \eta \frac{\pi (ka)^4 |I_0|^2}{12}$$

$$R_r = \eta \left(\frac{\pi}{6} \right) (ka)^4$$

For N-turns loop,

$$R_r = R_r = \eta \left(\frac{\pi}{6} \right) (ka)^4 N^2$$

- Loss resistance R_L ,

$$R_L = N \frac{a}{b} R_s,$$

where b is the wire radius, and R_s is the conductor surface impedance.

Increasing the number of turns, increases the antenna radiation efficiency.