# Topic 3 <br> Fundamental Parameters of Antennas 

Tamer Abuelfadl

Electronics and Electrical Communications Department
Faculty of Engineering
Cairo University

## Electromagnetic Radiation

Time-changing current radiates and accelerated charge radiates.



## Fundamental Parameters of Antennas

(1) Radiation Pattern

- Radiation Pattern Lobes
- Isotropic, Directional, and Omnidirectional Pattern
- Principal Patterns
- Field Regions
- Solid Angle
(2) Radiation Power Density
(3) Radiation Intensity
(4) Beamwidth
(5) Directivity
(6) Beam Solid Angle $\Omega_{A}$ (Beam Area)
(7) Antenna Input Impedance and Radiation Efficiency
(8) Antenna Gain

Many of the definitions of these terms are taken from the IEEE Std 145-1993.

## Outline

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## Radiation Patterns

## Antenna Radiation Pattern or Antenna Pattern

The spatial distribution of a quantity that characterizes the electromagnetic field generated by an antenna.

- Radiation is a spherical

TEM fields with
propagation in âr
direction and fields in $\hat{a}_{\theta}$
and $\hat{\mathbf{a}}_{\phi}$ directions.

- $\left|E_{\theta}\right|$ and $\left|E_{\phi}\right| \propto 1 / r$
- $\left|E_{\theta}\right|$
- $\left|F_{\phi}\right|$
- Phases of these fields, $\delta_{\theta}$ and $\delta_{\phi}$.


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## Radiation Patterns

- Field Pattern: A plot of the field magnitude $(|\mathbf{E}|$ or $|\mathbf{H}|)$ on a linear scale.
- Power Pattern: A plot of the square of the field magnitude $\left(|\mathbf{E}|^{2}\right.$ or $\left.|\mathbf{H}|^{2}\right)$ on either a linear or decibel $(\mathrm{dB}, 20 \log |\mathbf{E}|)$.


Field Pattern
Linear Scale


Power Pattern
Linear Scale

Decibel Scale (dB)

## Radiation Patterns

## Radiation Pattern Lobes

- Major lobe
- Minor lobes
- Side lobe
- Back lobe



## Radiation Patterns

## Isotropic, Directional, and Omnidirectional Pattern

## Isotropic radiator

a hypothetical lossless antenna having equal radiation in all directions.

## Directional antenna

having the property of radiating or receiving electromagnetic waves more effectively in some directions than in others, usually applied on antennas having directivity greater than that of half-wave dipole.

## Omnidirectional pattern

having an essentially nondirectional pattern in a given plane.


Omnidirectional in azimuth

## Radiation Patterns

## Principal Patterns

## E-Plane <br> H-Plane

The plane containing the electric-field The plane containing the vector and the direction of maximum magnetic-field vector and the radiation. direction of maximum radiation.


## Radiation Patterns

## Field Regions

- Reactive near field region:

Far-field (Fraunhofer)
reactive fields predominates radiating fields.

- Radiating near field (Fresnel) region: radiation fields predominates, but the radiation pattern varies with the radius $r$.
- Far-field (Fraunhover) region:
- Fields vary as $\frac{e^{-j k r}}{r}$, and the radiation pattern is independent on $r$.
- Electric and magnetic fields are predominantly in $\mathbf{a}_{\theta}$ and $\mathbf{a}_{\phi}$ directions, and are in phase.

Radiating near-field (Fresnel) region


## Radiation Patterns

Solid Angle (Steradian)


$$
\begin{gathered}
d A=r^{2} \sin \theta d \theta d \phi, \quad d \Omega=\frac{d A}{r^{2}}=\sin \theta d \theta d \phi \\
\Omega=\iint_{(\theta, \phi)} \sin \theta d \theta d \phi \quad(\mathrm{sr})
\end{gathered}
$$

## Radiation Patterns

## Solid Angle (Steradian)

For a sphere of radius $r$, find the solid angle $\Omega_{A}$ (in square radians or steradians) of a spherical cap on the surface of the sphere over the north-pole region defined by a spherical angle of $0 \leq \theta \leq 30^{\circ}, 0 \leq \phi \leq 360^{\circ}$.

## Solution



## Radiation Patterns

Solid Angle (Steradian)

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## Solution

$$
\begin{aligned}
\Omega_{A} & =\int_{0}^{2 \pi} \int_{0}^{\pi / 6} d \Omega=\int_{0}^{2 \pi} \int_{0}^{\pi / 6} \sin \theta d \theta d \phi=\int_{0}^{2 \pi} d \phi \int_{0}^{\pi / 6} \sin \theta d \theta \\
& =2 \pi[-\cos \theta]_{0}^{\pi / 6}=2 \pi\left[-\frac{\sqrt{3}}{2}+1\right]=0.83566 \quad \text { (sr) }
\end{aligned}
$$

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8. Antenna Gain

## Radiation Power Density

## Instantaneous Poynting Vector

$$
\mathscr{W} \text { or } S=\mathscr{E} \times \mathscr{H}
$$

$\mathscr{W}$ or $S=$ instantaneous Poynting vector $\left(\mathrm{W} / \mathrm{m}^{2}\right)$.
$\mathscr{E}=$ instantaneous electric-field intensity (V/m). $\mathscr{H}=$ instantaneous magnetic-field intensity (A/m).

$$
\mathscr{P}=\oiint_{S} \mathscr{W} \cdot d \mathbf{s}=\oiint_{S} \mathscr{W} \cdot \hat{\mathbf{a}}_{n} d a
$$

$\mathscr{P}=$ instantaneous total power (W)

## Radiation Power Density

$$
\begin{gathered}
\mathscr{E}(x, y, z ; t)=\mathfrak{R}\left[\mathbf{E}(x, y, z) e^{j \omega t}\right]=\frac{1}{2}\left[\mathbf{E} e^{j \omega t}+\mathbf{E}^{*} e^{-j \omega t}\right] \\
\mathscr{H}(x, y, z ; t)=\mathfrak{R}\left[\mathbf{H}(x, y, z) e^{j \omega t}\right]=\frac{1}{2}\left[\mathbf{H} e^{j \omega t}+\mathbf{H}^{*} e^{-j \omega t}\right] \\
\mathscr{W} \text { or } \boldsymbol{S}=\mathscr{E} \times \mathscr{H}=\frac{1}{2} \Re\left[\mathbf{E} \times \mathbf{H}^{*}\right]+\frac{1}{2} \Re\left[\mathbf{E} \times \mathbf{H} e^{j 2 \omega t}\right]
\end{gathered}
$$

## Average Poynting Vector

$$
\mathbf{W}_{\mathrm{av}}(x, y, z) \text { or } \mathbf{S}_{\mathrm{av}}(x, y, z)=\frac{1}{2} \mathfrak{R}\left[\mathbf{E} \times \mathbf{H}^{*}\right]
$$

$$
\begin{aligned}
P_{\mathrm{rad}} & =\oiint_{S} \mathbf{W}_{\mathrm{rad}} \cdot d \mathbf{s}=\oiint_{S} \mathbf{W}_{\mathrm{av}} \cdot \hat{\mathrm{n} d a} \\
& =\oiint_{S} \frac{1}{2} \Re\left[\mathbf{E} \times \mathbf{H}^{*}\right] \cdot d \mathbf{s}
\end{aligned}
$$

where $P_{\mathrm{rad}}$ is the average radiated power.

## Radiation Power Density

## Example 2.2

The radial component of the radiated power density (Poynting vector radial component) of an antenna is given by,

$$
\mathrm{W}_{\mathrm{rad}}=\hat{\mathbf{a}}_{r} W_{r}=\hat{\mathbf{a}}_{r} A_{0} \frac{\sin \theta}{r^{2}} \quad\left(\mathrm{~W} / \mathrm{m}^{2}\right)
$$

Determine the total radiated power.

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$$

Determine the total radiated power．
Solution：

$$
\begin{align*}
P_{\mathrm{rad}} & =\oiint_{S} \mathbf{W}_{\mathrm{rad}} \cdot \hat{\mathbf{n}} d a \\
& =\int_{0}^{2 \pi} \int_{0}^{\pi}\left(\hat{\mathbf{a}}_{r} A_{0} \frac{\sin \theta}{r^{2}}\right) \cdot\left(\hat{\mathbf{a}}_{r} r^{2} \sin \theta d \theta d \phi\right)=\pi^{2} A_{0} \tag{W}
\end{align*}
$$

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## Radiation Intensity

## Radiation Intensity

The power radiated from an antenna per unit solid angle,

$$
U=r^{2} W_{\mathrm{rad}} \quad(\mathrm{~W} / \text { unit solid angle })
$$

$$
\begin{aligned}
U(\theta, \phi)=\frac{r^{2}}{2 \eta}|\mathbf{E}(r, \theta, \phi)|^{2} & =\frac{r^{2}}{2 \eta}\left[\left|E_{\theta}(r, \theta, \phi)\right|^{2}+\left|E_{\phi}(r, \theta, \phi)\right|^{2}\right] \\
& =\frac{1}{2 \eta}\left[\left|E_{\theta}^{\circ}(\theta, \phi)\right|^{2}+\left|E_{\phi}^{\circ}(\theta, \phi)\right|^{2}\right]
\end{aligned}
$$

where far-zone electric field of the antenna,

$$
\mathbf{E}(r, \theta, \phi)=\left[E_{\theta}^{\circ}(\theta, \phi) \hat{\mathbf{a}}_{\theta}+E_{\phi}^{\circ}(\theta, \phi) \hat{\mathbf{a}}_{\phi}\right] \frac{e^{-j k r}}{r}
$$

## Radiation Intensity

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The power radiated from an antenna per unit solid angle,

$$
\begin{gathered}
U=r^{2} W_{\mathrm{rad}} \quad \text { (W/unit solid angle) } \\
P_{\mathrm{rad}}=\oiint_{\Omega} U d \Omega=\int_{0}^{2 \pi} \int_{0}^{\pi} U \sin \theta d \theta d \phi
\end{gathered}
$$

## Radiation from an isotropic source

$$
\begin{aligned}
P_{\mathrm{rad}}=\oiint_{\Omega} U_{0} d \Omega & =U_{0} \oiint_{\Omega} d \Omega=4 \pi U_{0} \\
U_{0} & =\frac{P_{\mathrm{rad}}}{4 \pi}
\end{aligned}
$$

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## Beamwidth

- HPBW (Half Power Beam Width)
- FNBW (First-Null Beam Width)



## Beamwidth

## Example 2.4

The normalized radiation intensity of an antenna is represented by,

$$
U(\theta)=\cos ^{2}(\theta) \cos ^{2}(3 \theta), \quad\left(0 \leq \theta \leq 90^{\circ}, \quad 0 \leq \phi \leq 360^{\circ}\right)
$$

(1) Find the HPBW
(2) Find the FNBW
(1) $U\left(\theta_{h}\right)=\cos ^{2}\left(\theta_{h}\right) \cos ^{2}\left(3 \theta_{h}\right)=0.5 \Longrightarrow \cos \left(\theta_{h}\right) \cos \left(3 \theta_{h}\right)=0.707$ $\theta_{h}=\cos ^{-1}\left(\frac{0.707}{\cos 3 \theta_{h}}\right)$, iteratively gives $\quad \theta_{h} \approx 0.251 \mathrm{rad}=14.3725$ $\mathrm{HPBW}=2 \theta_{h} \approx 0.502 \mathrm{rad}=28.745^{\circ}$
(3) $U\left(\theta_{n}\right)=\cos ^{2}\left(\theta_{n}\right) \cos ^{2}\left(3 \theta_{n}\right)=0$
$\theta_{n}=\frac{\pi}{6} \mathrm{rad}=30^{\circ}$


## Beamwidth

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(2) $U\left(\theta_{n}\right)=\cos ^{2}\left(\theta_{n}\right) \cos ^{2}\left(3 \theta_{n}\right)=0$

$$
\theta_{n}=\frac{\pi}{6} \mathrm{rad}=30^{\circ}
$$

$\mathrm{FNBW}=2 \theta_{n}=\frac{\pi}{3} \mathrm{rad}=60^{\circ}$

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## Directivity

## Directivity

The ratio of the radiation intensity in a given direction to the radiation intensity averaged over all directions.

If the direction is not specified the direction of the maximum radiation intensity is implied.

$$
\begin{gathered}
D=\frac{U}{U_{0}}=\frac{4 \pi U}{P_{\mathrm{rad}}} \\
D_{\max }=D_{0}=\frac{U_{\mathrm{max}}}{U_{0}}=\frac{4 \pi U_{\max }}{P_{\mathrm{rad}}}
\end{gathered}
$$

- Partial Directivities $D_{\theta}$ and $D_{\phi}$,

$$
\begin{gathered}
D_{\theta}=\frac{4 \pi U_{\theta}}{\left(P_{\mathrm{rad}}\right)_{\theta}+\left(P_{\mathrm{rad}}\right)_{\phi}}, \quad D_{\phi}=\frac{4 \pi U_{\phi}}{\left(P_{\mathrm{rad}}\right)_{\theta}+\left(P_{\mathrm{rad}}\right)_{\phi}} \\
D=D_{\theta}+D_{\phi}
\end{gathered}
$$

## Directivity

## Example 2.6

The radial component of the radiated power density of an infinitesimal linear dipole of length $I \ll \lambda$ is given by,

$$
\mathrm{W}_{\mathrm{av}}=\hat{\mathbf{a}}_{r} W_{r}=\hat{\mathbf{a}}_{r} A_{0} \frac{\sin ^{2} \theta}{r^{2}}
$$

Determine the maximum directivity of the antenna and express the directivity as a function of $\theta$ and $\phi$.

## Directivity

## Example 2.6

The radial component of the radiated power density of an infinitesimal linear dipole of length $I \ll \lambda$ is given by，

$$
\mathbf{W}_{\mathrm{av}}=\hat{\mathbf{a}}_{r} W_{r}=\hat{\mathbf{a}}_{r} A_{0} \frac{\sin ^{2} \theta}{r^{2}}
$$

Determine the maximum directivity of the antenna and express the directivity as a function of $\theta$ and $\phi$ ．

Solution：

$$
\begin{gathered}
U=r^{2} W_{r}=A_{0} \sin ^{2} \theta \\
P_{\mathrm{rad}}=\int_{0}^{2 \pi} \int_{0}^{\pi} A_{0} \sin ^{2} \theta \sin \theta d \theta d \phi=A_{0}\left(\frac{8 \pi}{3}\right) \\
D=\frac{4 \pi U}{P_{\mathrm{rad}}}=1.5 \sin ^{2} \theta \\
D_{\max }=1.5 \quad \text { at } \theta=90^{\circ}
\end{gathered}
$$

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## Beam Solid Angle $\Omega_{A}$ (Beam Area)

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The solid angle through which all the power of the antenna would flow if its radiation is constant (and equal to the maximum value of $U$ ) for all angles within $\Omega_{A}$.

$$
\Omega_{A}=\frac{P_{\mathrm{rad}}}{U_{\max }}=\frac{\oiint_{\Omega} U d \Omega}{U_{\max }}=\oiint_{\Omega} \frac{U}{U_{\max }} d \Omega=\frac{4 \pi}{D_{\max }}
$$

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## Antenna Input Impedance and Radiation Efficiency



- $R_{r}=$ radiation resistance of the antenna
- $R_{L}=$ loss resistance of the antenna
- $X_{A}=$ antenna reactance
- $Z_{g}=R_{g}+j X_{g}$ generator impedance
Antenna Input Impedance $Z_{A}$

$$
Z_{A}=R_{A}+j X_{A}, \quad R_{A}=R_{r}+R_{L}
$$

## Radiation Efficiency $\eta$

The ratio of the total power radiated by an antenna to the net power accepted by the antenna from the connected transmitter.

$$
\eta=\frac{P_{\mathrm{rad}}}{P_{\mathrm{Acc}}}=\frac{P_{\mathrm{rad}}}{P_{\mathrm{rad}}+P_{\text {losses }}}=\frac{R_{r}}{R_{A}}=\frac{R_{r}}{R_{r}+R_{L}}
$$

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## Antenna Gain

## gain (in a given direction)

The ratio of the radiation intensity, in a given direction, to the radiation intensity that would be obtained if the power accepted by the antenna were radiated isotropically.

- Gain does not include losses arising from impedance and polarization mismatches.
- If the direction is not specified, the direction of maximum radiation intensity is implied.

$$
G=\frac{4 \pi U}{P_{\text {Acc }}}=\eta D
$$

- Partial gains in $\theta$ and $\phi$ polarization:

$$
\begin{gathered}
G_{\theta}=\frac{4 \pi U_{\theta}}{P_{\mathrm{Acc}}}, \quad G_{\phi}=\frac{4 \pi U_{\phi}}{P_{\mathrm{Acc}}} \\
G=G_{\theta}+G_{\phi}
\end{gathered}
$$

