

# Small Signal Space Charge Modes in a Guiding Structure

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After some mathematical manipulations, we were able to reach to the following PDE that determines the axial electric field  $E_z$ .

$$\nabla_{\perp}^2 E_z + T^2 E_z = 0$$

where,

$$T^2 = \begin{cases} T_n^2 = (\gamma^2 - k^2) \left[ \frac{\beta_p^2}{(\beta_e - \gamma)^2} - 1 \right] & \text{inside the beam } r < b \\ -\tau_n^2 = -(\gamma^2 - k^2) & \text{outside the beam } b < r < a \end{cases} \quad (1)$$

$$E_z = \begin{cases} B J_0(T_n r), & \text{inside the beam } r < b \\ C I_0(\tau_n r) + D K_0(\tau_n r) & \text{outside the beam } b < r < a \end{cases}$$

$$\text{To satisfy the boundary conditions at } r = a, \quad \implies \quad E_z(r = a) = 0,$$

$$E_z = \begin{cases} B J_0(T_n r), & \text{inside the beam } r < b \\ C' [I_0(\tau_n r) K_0(\tau_n a) - K_0(\tau_n r) I_0(\tau_n a)] & \text{outside the beam } b < r < a \end{cases}$$

The other components of the fields can be obtained using Maxwell's equations,

$$\nabla \times \mathbf{E} = -j\omega\mu_0 H_{\phi} \hat{\mathbf{a}}_{\phi} \quad \implies \quad -j\gamma E_r - \frac{\partial E_z}{\partial r} = -j\omega\mu_0 H_{\phi}$$

$$\nabla \times \mathbf{H} = j\omega\epsilon_0 \mathbf{E} + J_z \hat{\mathbf{a}}_z, \quad \implies \quad j\gamma H_{\phi} = j\omega\epsilon_0 E_r$$

From these two equations,

$$H_{\phi} = \frac{-j\omega\epsilon_0}{k^2 - \gamma^2} \frac{\partial E_z}{\partial r}$$

$$H_{\phi} = \frac{-j\omega\epsilon_0}{k^2 - \gamma^2} \begin{cases} B T_n J_0'(T_n r) & \text{inside the beam } r < b \\ C \tau_n [I_0'(\tau_n r) K_0(\tau_n a) - K_0'(\tau_n r) I_0(\tau_n a)] & \text{outside the beam } b < r < a \end{cases}$$

Apply the continuity of  $E_z$  and  $H_{\phi}$  at  $r = b$ ,

$$\begin{aligned} B J_0(T_n b) &= C' [I_0(\tau_n b) K_0(\tau_n a) - K_0(\tau_n b) I_0(\tau_n a)] \\ B T_n J_0'(T_n b) &= C' \tau_n [I_0'(\tau_n b) K_0(\tau_n a) - K_0'(\tau_n b) I_0(\tau_n a)] \end{aligned}$$

Dividing these two equations,

$$T_n \frac{J_0'(T_n b)}{J_0(T_n b)} = \tau_n \frac{I_0'(\tau_n b) K_0(\tau_n a) - K_0'(\tau_n b) I_0(\tau_n a)}{I_0(\tau_n b) K_0(\tau_n a) - K_0(\tau_n b) I_0(\tau_n a)}$$

Using these identities,

$$J'_0(x) = -J_1(x), \quad I'_0(x) = I_1(x), \quad K'_0(x) = -K_1(x)$$

$$\boxed{T_n \frac{J_1(T_n b)}{J_0(T_n b)} = \tau_n \frac{I_1(\tau_n b) K_0(\tau_n a) + K_1(\tau_n b) I_0(\tau_n a)}{K_0(\tau_n b) I_0(\tau_n a) - I_0(\tau_n b) K_0(\tau_n a)}} \quad (2)$$

## Assumptions

We will assume the phase velocities almost equal to the velocity of the beam making  $\gamma \approx \beta_e$ , and hence  $\gamma \gg k$ . We can then use  $\beta_e$  instead of  $\gamma$  in Eq. (1) (except in the denominator term), with the result,

$$\tau_n \approx \beta_e \quad (3)$$

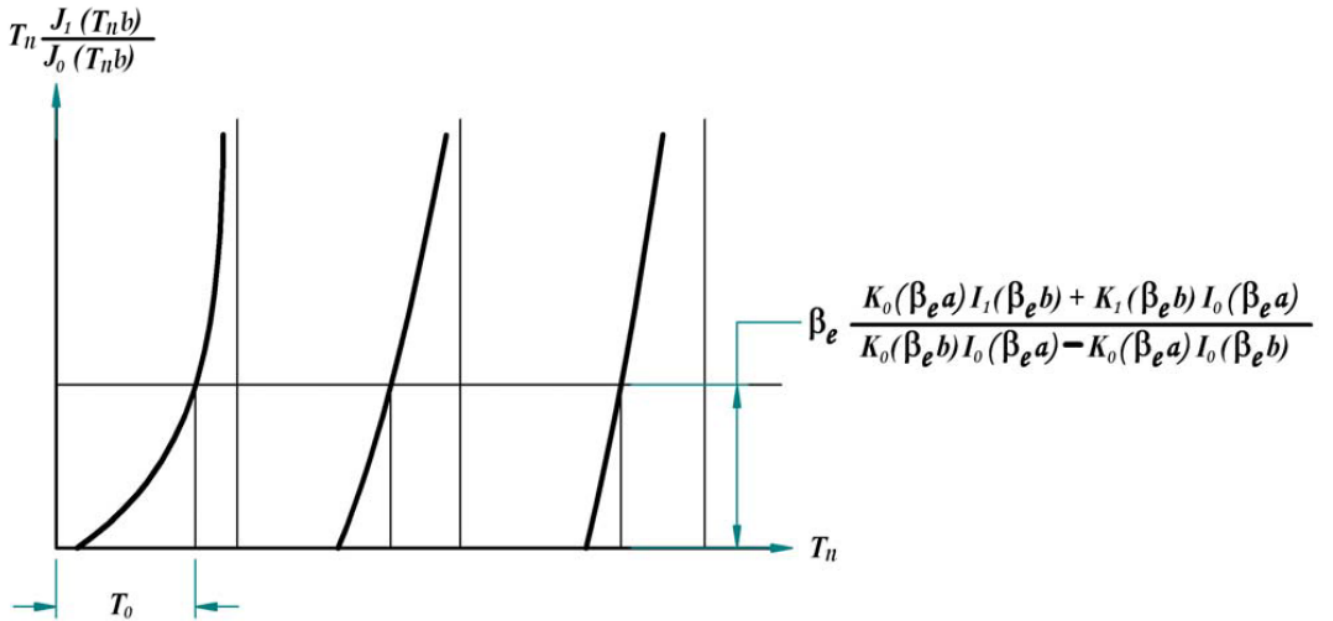
$$T_n \approx \beta_e \left[ \frac{\beta_p^2}{(\beta_e - \gamma)^2} - 1 \right], \quad \implies \quad \gamma = \beta_e \pm \beta_q = \beta_e \pm \frac{\beta_p}{\sqrt{1 + \frac{T_n^2}{\beta_e^2}}}$$

The plasma reduction factor  $R$  is defined as,

$$R = \frac{\beta_q}{\beta_p} = \frac{1}{\sqrt{1 + \frac{T_n^2}{\beta_e^2}}},$$

where  $T_n$  is obtained by solving equation (2), after using the approximation Eq. (3),

$$\boxed{T_n \frac{J_1(T_n b)}{J_0(T_n b)} = \beta_e \frac{I_1(\beta_e b) K_0(\beta_e a) + K_1(\beta_e b) I_0(\beta_e a)}{K_0(\beta_e b) I_0(\beta_e a) - I_0(\beta_e b) K_0(\beta_e a)}} \quad (4)$$



The dispersion relation can be written in normalized form as,

$$\boxed{(T_n b) \frac{J_1(T_n b)}{J_0(T_n b)} = (\beta_e b) \frac{I_1(\beta_e b) K_0\left(\beta_e b \frac{a}{b}\right) + K_1(\beta_e b) I_0\left(\beta_e b \frac{a}{b}\right)}{K_0(\beta_e b) I_0\left(\beta_e b \frac{a}{b}\right) - I_0(\beta_e b) K_0\left(\beta_e b \frac{a}{b}\right)}} \quad (5)$$

This dispersion equation is solved for the different modes  $T_n b$  for the two input independent variables  $\beta_e b$  and  $\frac{a}{b}$ , and the plasma reduction factor is given as,

$$R = \frac{\beta_q}{\beta_p} = \frac{1}{\sqrt{1 + \left(\frac{T_n b}{\beta_e b}\right)^2}},$$